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# Earthquake Rupture Modeling: Fracturing vs. Friction

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### **Motivation**





Joint theory of friction and fracturing for induced earthquakes:

Mineralization of parts of the fault, slip propagation includes breaking of locked sections (fault jogs and step overs) – fracturing along with frictional sliding on preexisting surfaces.

Computational complexity of rate-and-state and unclear physics behind the fitting parameters: Can we approximate rate-and-state dynamic rupture propagation results with something simpler: EPFM or slip-weakening friction?

### **Problem and solution**



### **Problem:**

Absence of joint theory of fracturing and friction that would be able to describe both brittle cracking and frictional sliding along the fault and delineate where the two are applicable.

### **Solution:**

- Finite element numerical simulations
- Observing similarities and differences in stress, slip, friction coefficient, slip rate etc., trying to link fracture and friction theories
- Comparison with experimental results?

### Earthquake cycle model





- 2D, plane strain
- Linear elastic material
- Boundary conditions: lithostatic compression and shear
- 3 fault sections: middle section – static friction  $\mu = 0.6$ ; sides – slip-weakening  $\mu_d = 0.6$ ,  $\mu_s =$ 0.65
- Time scale: years for quasistatic part, seconds for dynamic part

Figure 3. Model geometry

## Quasi-static cycle

- 3 cycles.
- Fault healing is enforced between the cycles.



Figure 4. Shear stress on the fault



#### Figure 5. Slip on the fault





### **Slip-weakening friction vs. fracturing**

Fracture? Exponential cohesive zone



$$\mu = \mu_d + (\mu_s - \mu_d) \frac{(D + D_1)}{D_2} e^{1 - \frac{(D + D_1)}{D_2}}$$



**Slip-weakening** 

$$\mu = \begin{cases} \mu_s - (\mu_s - \mu_d) \frac{D}{D_c} & D \le D_c \\ \mu_d & D > D_c \end{cases}$$

**Rate-and-state** 

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$$\mu = \mu_0 + aln\left(\frac{V}{V_0}\right) + bln\left(\frac{V_0\theta}{L}\right)$$
$$\dot{\theta} = 1 - \frac{V\theta}{L}$$

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• Slip distribution for dynamic rupture propagation

**Fracture**  $G_{IIC} = 46.85$ 

**Slip-weakening**  $\mu_s = 0.65, \ \mu_d = 0.6, \ D_c = 2.5e - 5$ 

#### **Rate-and-state**

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a = 0.0029, b = 0.0043,

 $D_c = 0.2047e - 5, \ \mu_0 = 0.6145$ 



Figure 6. Slip on the fault

• Slip rate distribution for dynamic rupture propagation



Figure 7. Slip rate on the fault

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Shear stress on the fault for dynamic rupture propagation 

 $G_{IIC} = 46.85$ 

Fracture

**Slip-weakening**  $\mu_s = 0.65, \, \mu_d = 0.6, \, D_c = 2.5e - 5$ 





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a = 0.0029, b = 0.0043,

 $D_c = 0.2047e - 5, \ \mu_0 = 0.6145$ 



Figure 8. Shear stress on the fault



Rupture velocity and tip location for dynamic rupture propagation



Figure 9. Rupture tip velocity and location

### **Quantitative comparison - energy**

• Energy determined as the area under the stress vs. slip curve:



Figure 10. Fracture energy

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- Quasi-static models of earthquake cycle (slip-weakening instability) with fault healing between the cycles
- Dynamic part of the cycle modeled with Pylith slip-weakening subroutine; Pylith rate-and-state subroutine and a custom exponential cohesive zone model (fracture?)
- Exponential cohesive zone vs. slip-weakening vs. rate-and-state dynamic part:
  - Far field: very similar (virtually indistinguishable) observations for the specific case of equal fracture energies
  - Near field: minor differences in stress profiles, slip rates and slip distributions. Resolvable with experiments?
- These models can yield very different results if we don't actively fit parameters to obtain the same fracture energy

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# Work in progress

• Parametric studies: which model better reproduces specific earthquake / experimental observations? Are parameters used for fitting within physical range?

- Analytical expression for rate-and-state "fracture energy"
- Experiments on glued polycarbonate

$$G_c = \frac{\sigma b D_c}{2} \left[ \ln \left( \frac{V \theta_i}{D_c \Omega} \right) \right]^2 \qquad \Omega \equiv \frac{V \theta}{D_c}$$



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### **Questions?**

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