

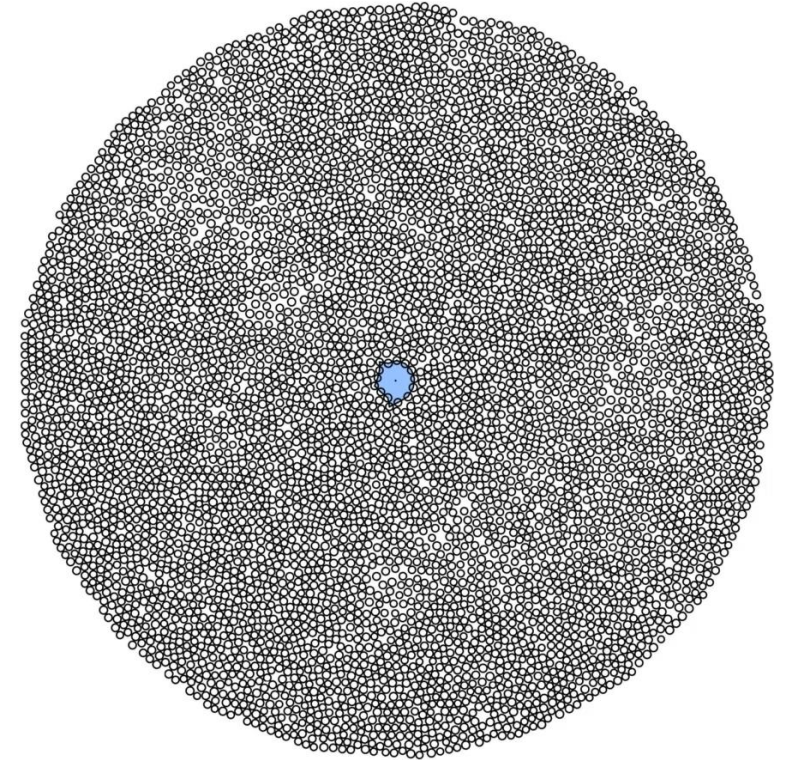
# Jamming transition and emergence of fracturing

## In wet granular media

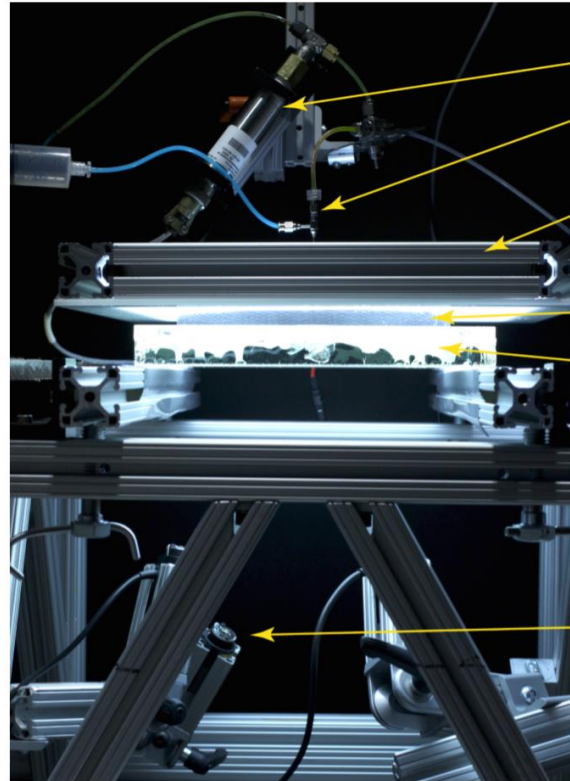
ERL Annual Meeting

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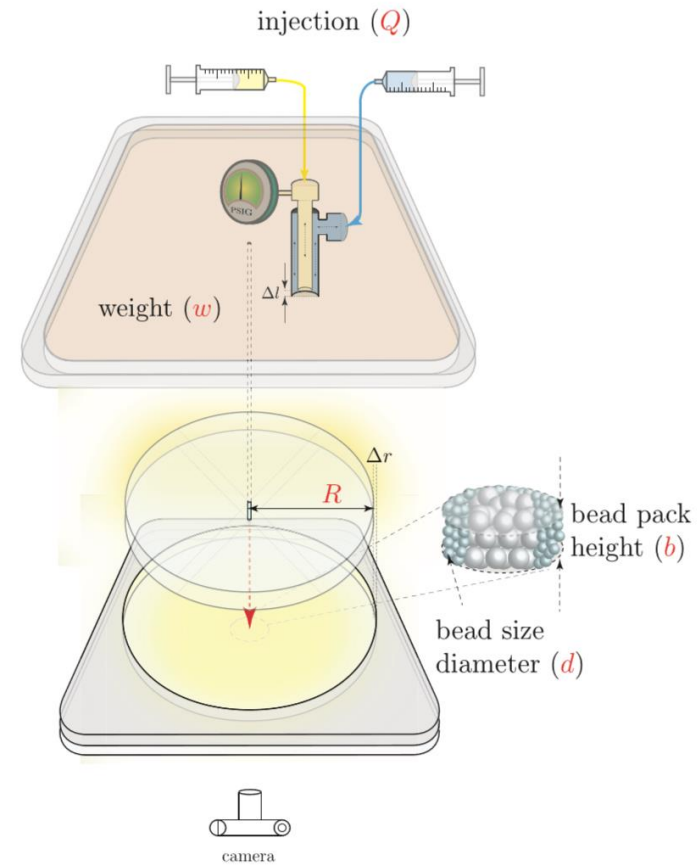
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- 2. State Key Laboratory of Wat. Resour. and Hydropower Eng. Sci., Wuhan University**
- 3. Department of Civil Engineering, HKU**



# Experiments phase diagram: wettability and granular fracture



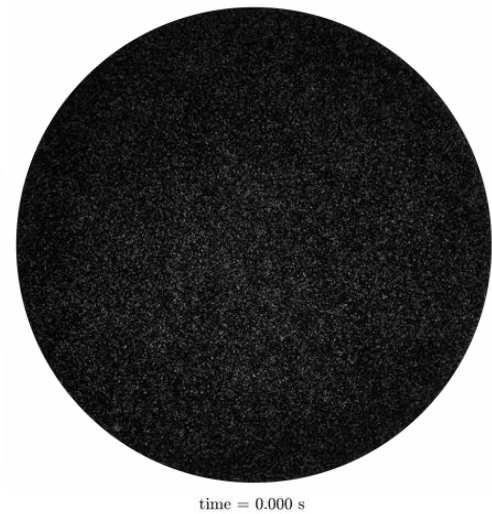
pressure sensor  
coaxial injector  
framed LED-light panel  
top-lid  
base plate  
UV-LED light



Trojer et al. (*in review*).

# Experiments phase diagram: wettability and granular fracture

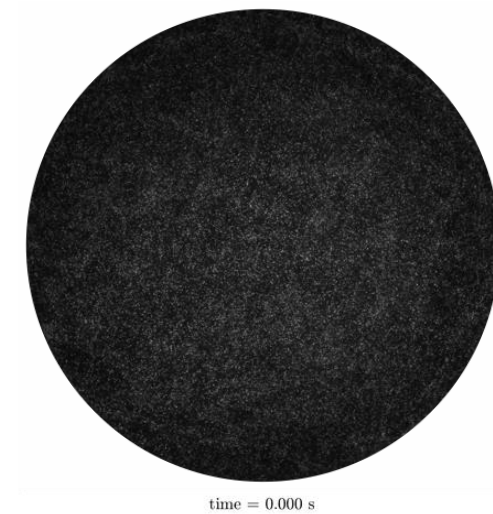
silicone oil – glycerol



water – silicone oil

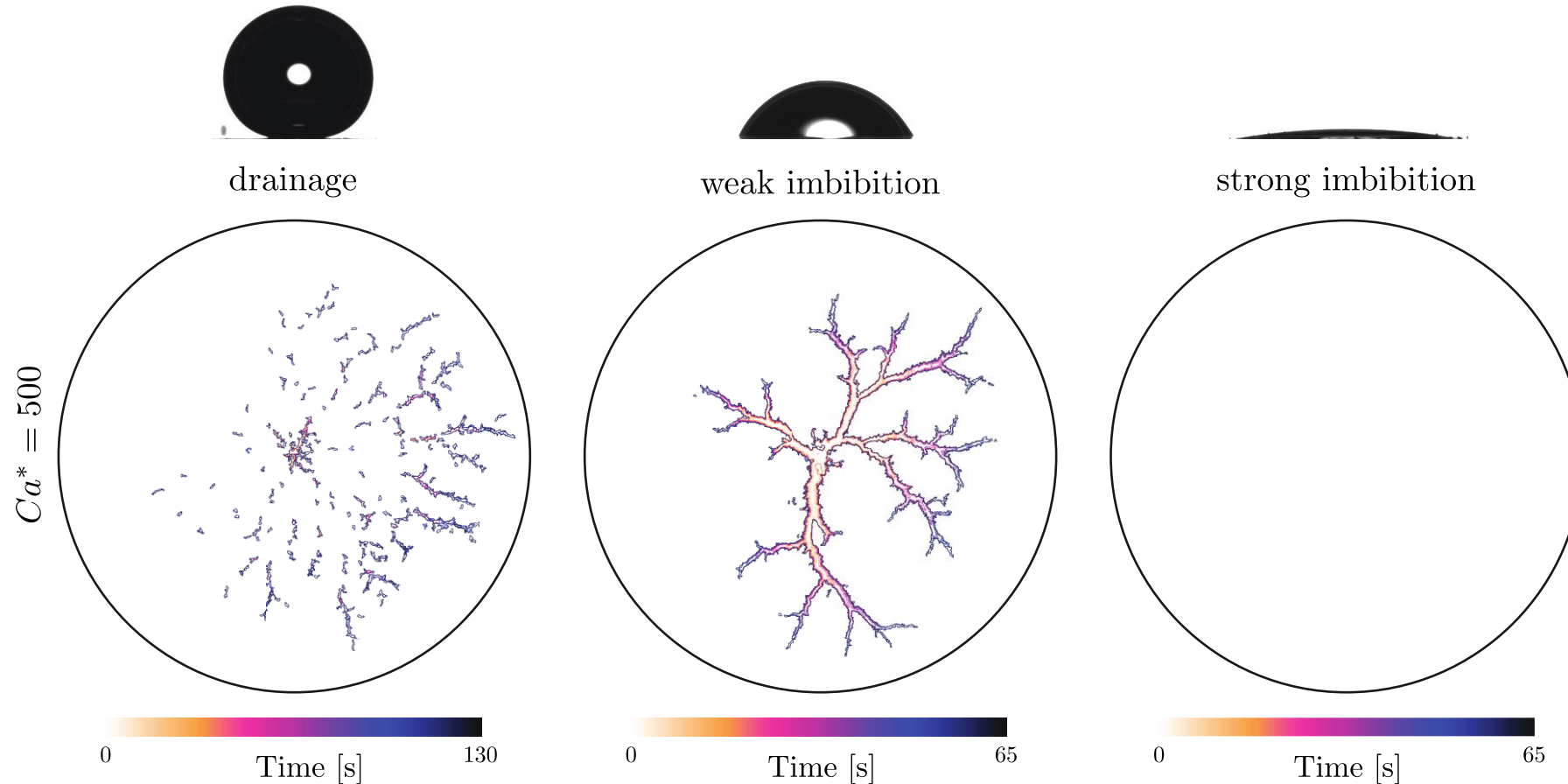


water – fluorinated oil



Trojer et al. (*in review*).

# Experiments phase diagram: wettability and granular fracture



Trojer et al. (*in review*).

# Coupling of multiphase flow and grain mechanics

## □ Discrete element modeling (DEM) framework:

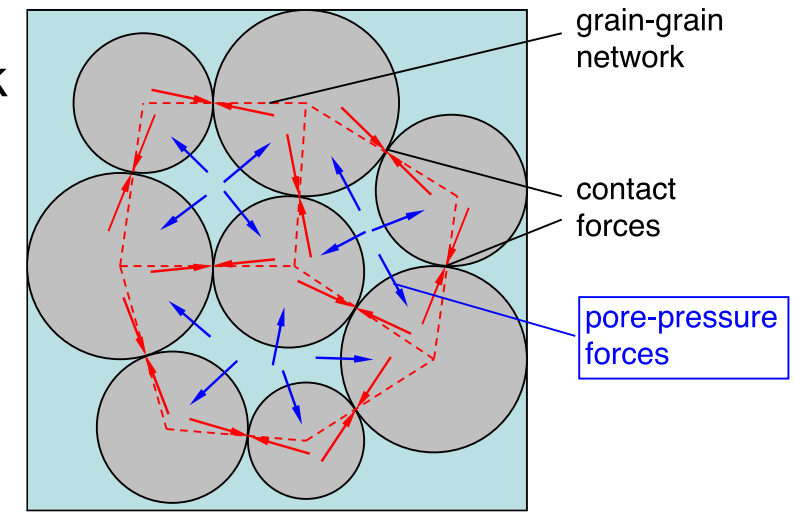
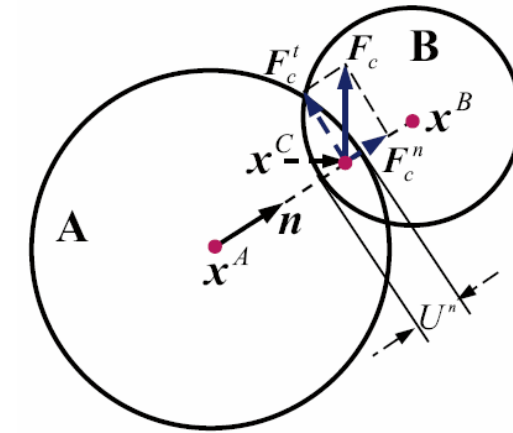
- Simulate particle interactions solving Newton's law of motion

$$m_i \ddot{\mathbf{x}}_i = \sum_j \mathbf{F}_{ij} \quad \mathbf{I}_i \ddot{\theta}_i = \sum_j \mathbf{M}_{ij}$$

- Define dual networks: grain-contact network and pore network

## □ Two-way coupling:

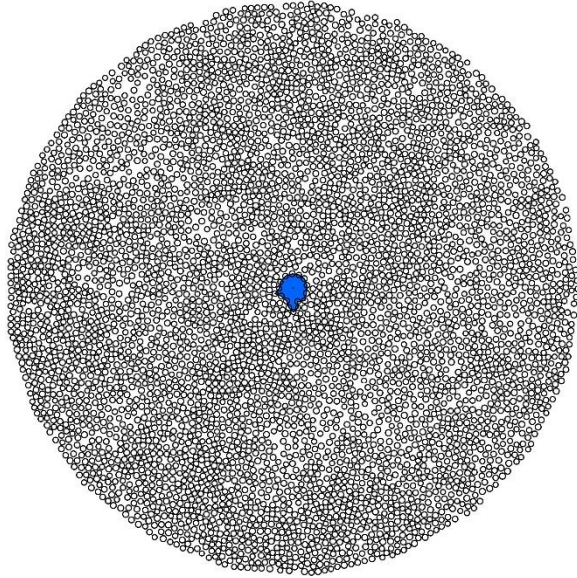
- Pressure (from both fluids) exert forces on particles
- Particle rearrangement causes volume and pressure changes



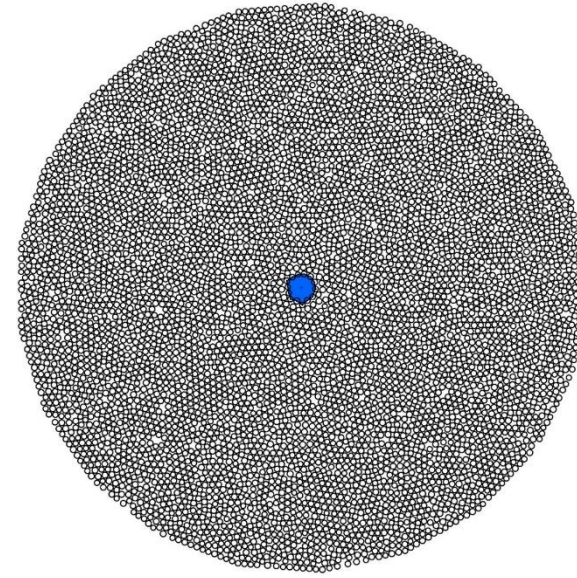
Primkulov et al. *JFM* (2019).  
Primkulov et al. *PRF* (2018).

# Simulation setup: frictional granular pack

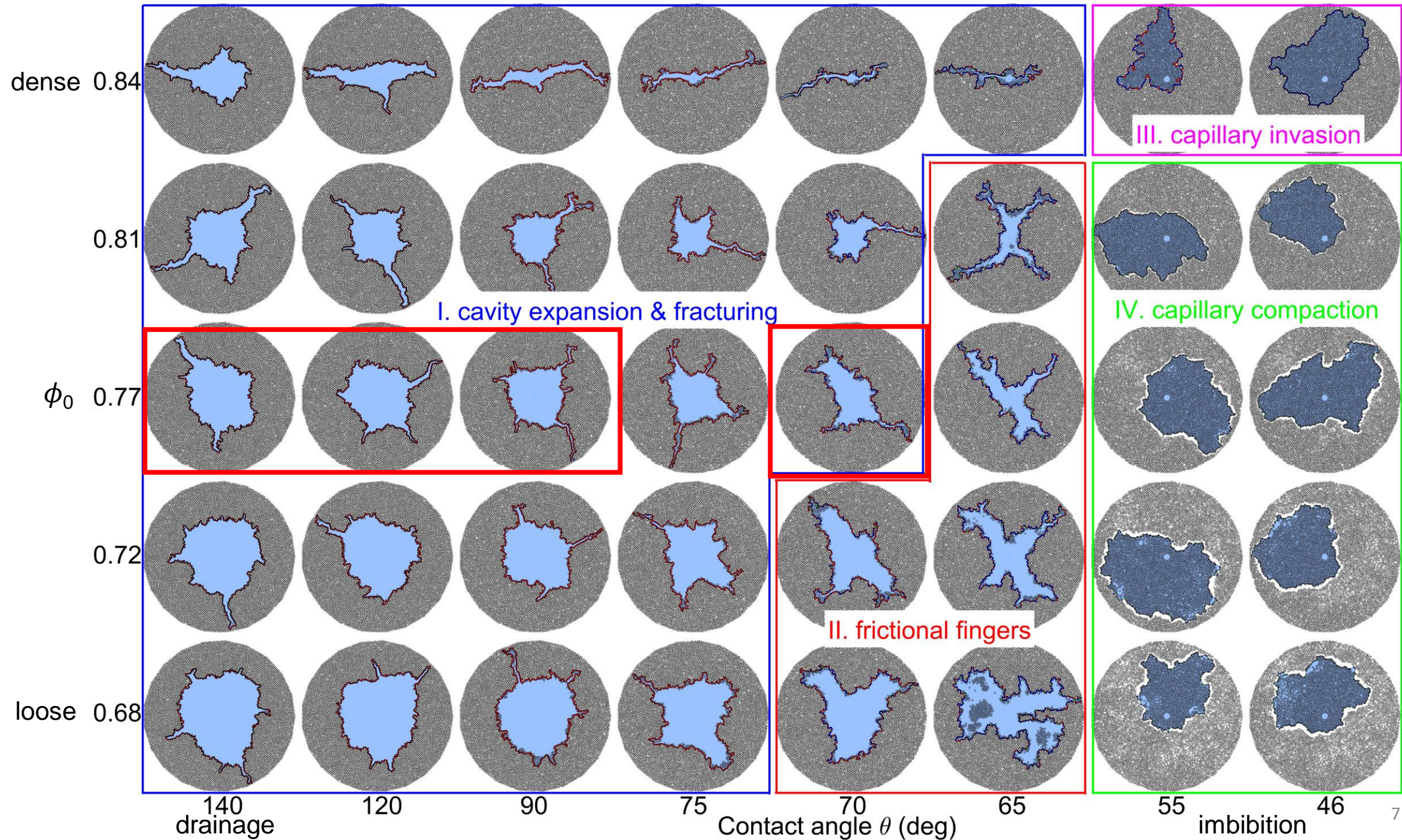
$\phi_0 = 0.68$  (loose)



$\phi_0 = 0.84$  (dense)

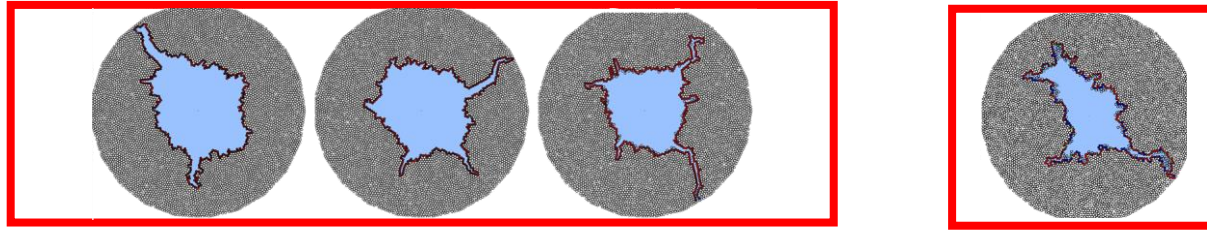


- Contact angle  $\theta = 140^\circ$  (drainage) -  $90^\circ$  (neutral) -  $46^\circ$  (imbibition)
- Initial packing density  $\phi_0 = 0.68$  (loose) -  $0.84$  (dense)
- Coefficient of friction  $\mu = 0.3$
- $Ca^* = 0.5$ ,  $Q = 4.29 \times 10^{-11} \text{ m}^3/\text{s} \rightarrow \Delta P_{viscous} \approx 0.001 \Delta P_{capillary} \rightarrow$  capillary-dominated regime

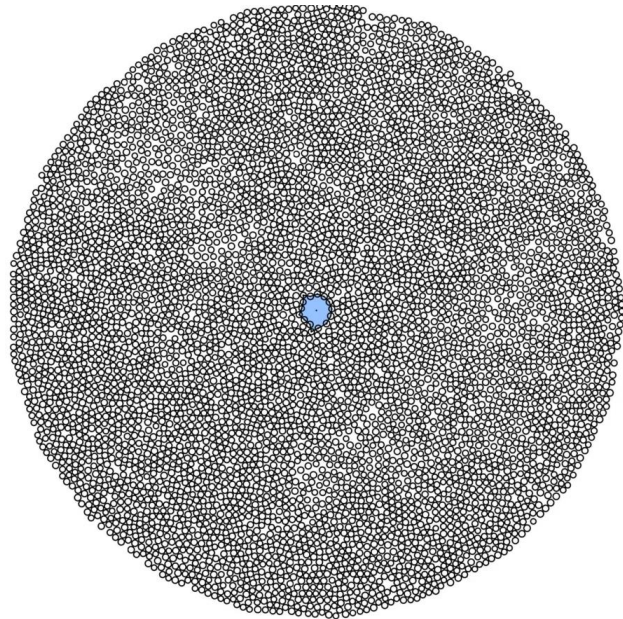


# Evolution of interface morphology

$$\phi_0 = 0.77$$

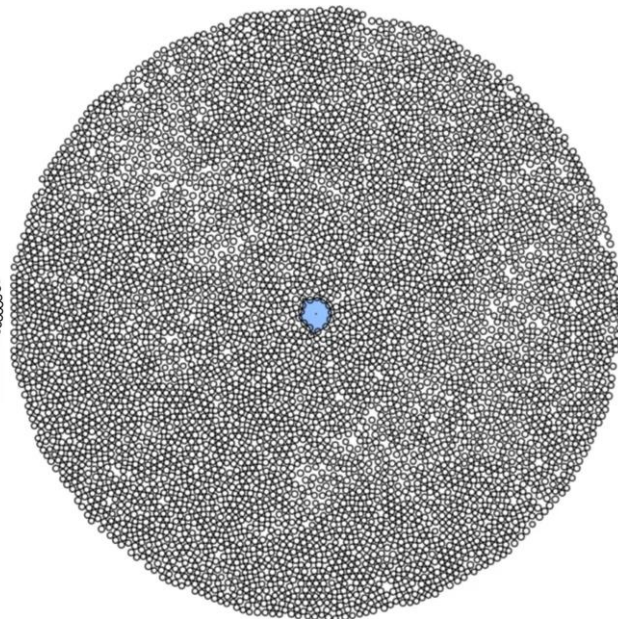


$\theta = 140^\circ$

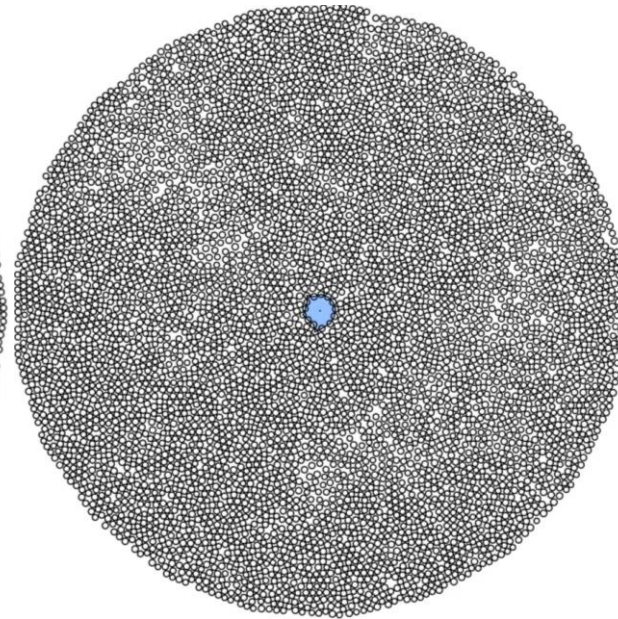


drainage

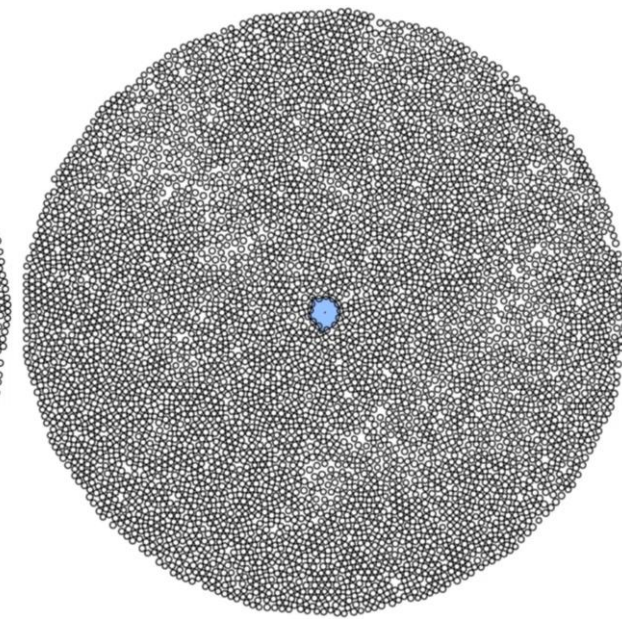
$\theta = 120^\circ$



$\theta = 90^\circ$



$\theta = 70^\circ$



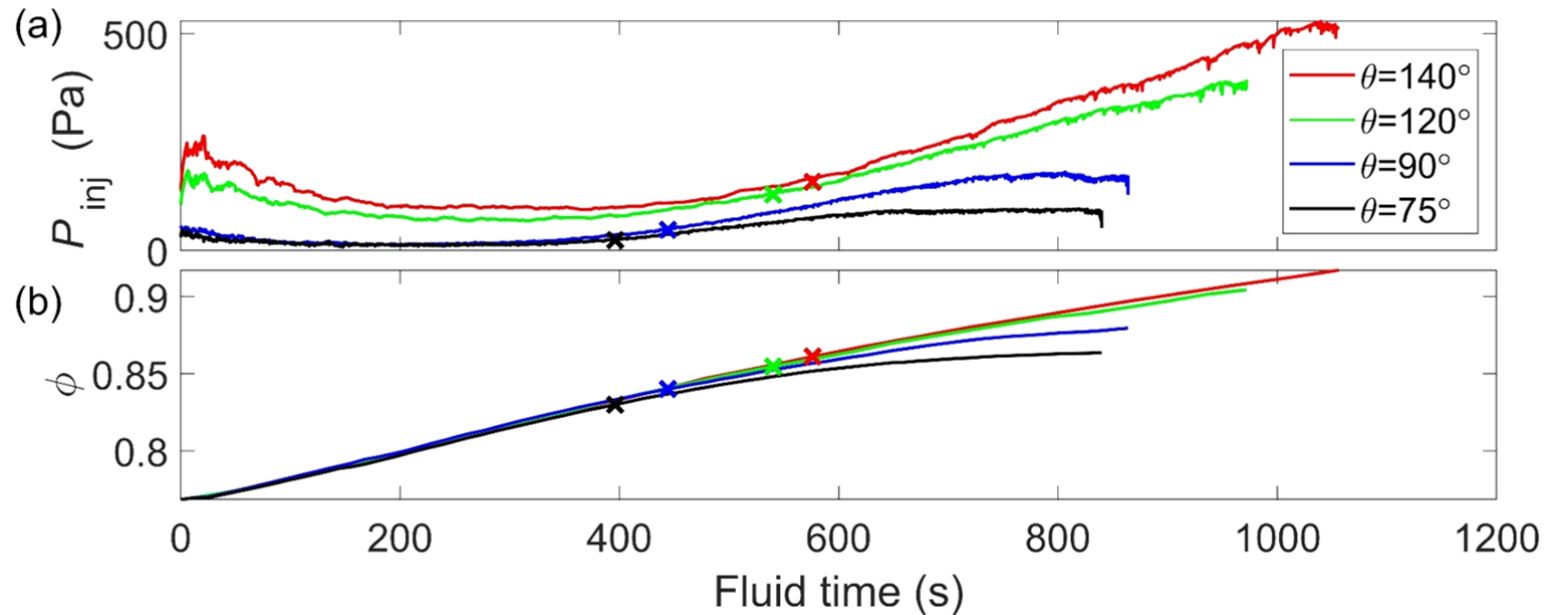
imbibition

□ **Key observation:** contact angle impacts the onset of fracturing – imbibition promotes fracture



# What causes the transition from cavity expansion to fracturing?

- The injection pressure by itself, or packing fraction by itself, do not explain the transition



- We hypothesize that this is akin to a phase transition from liquid-like to solid-like behavior

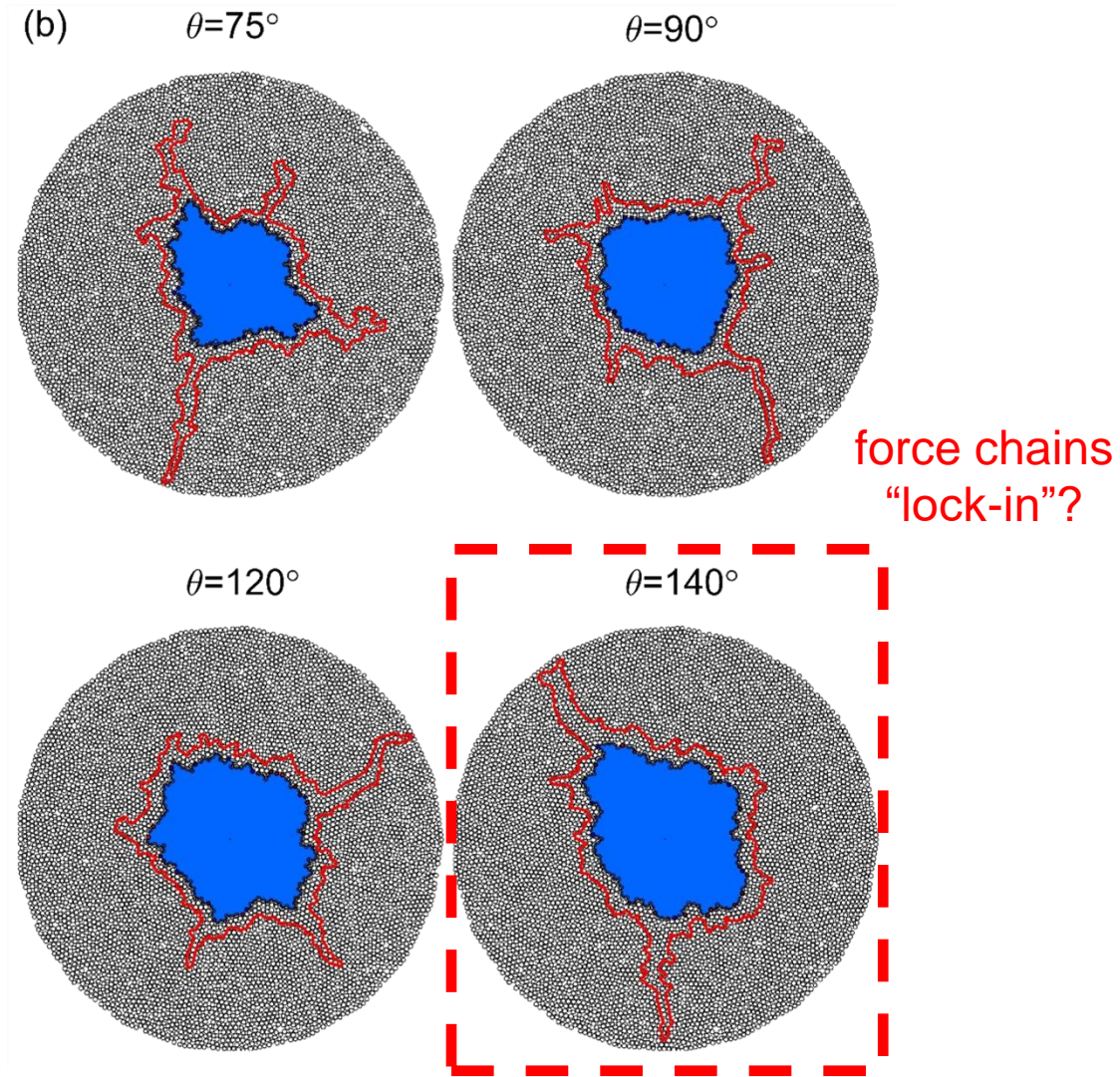
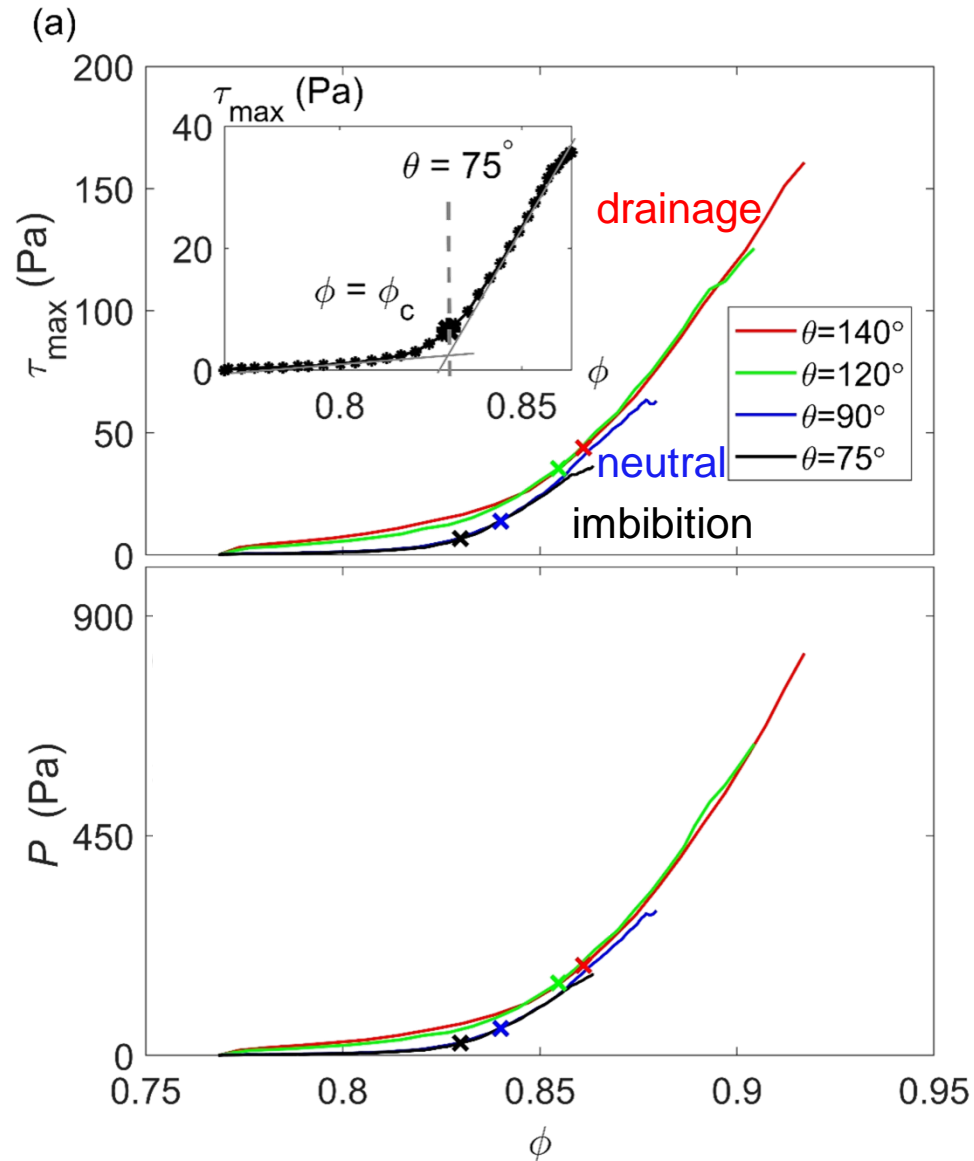
→ **A jamming transition**

- Can be characterized by the mean contact number  $Z$  or the mean particle stress  $P$

(Majmudar et al., *PRL* 2007)

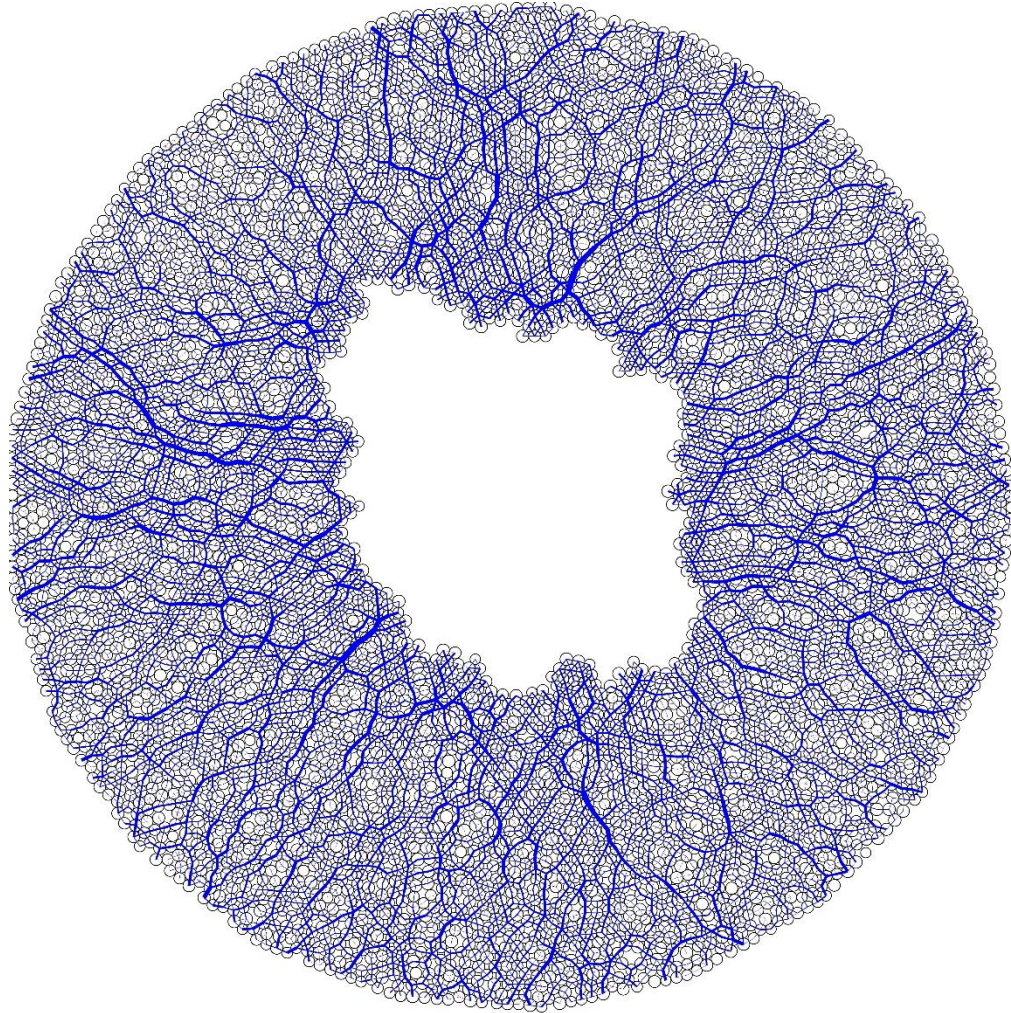
# Fracture initiation at the jamming transition

$\phi_0 = 0.77$



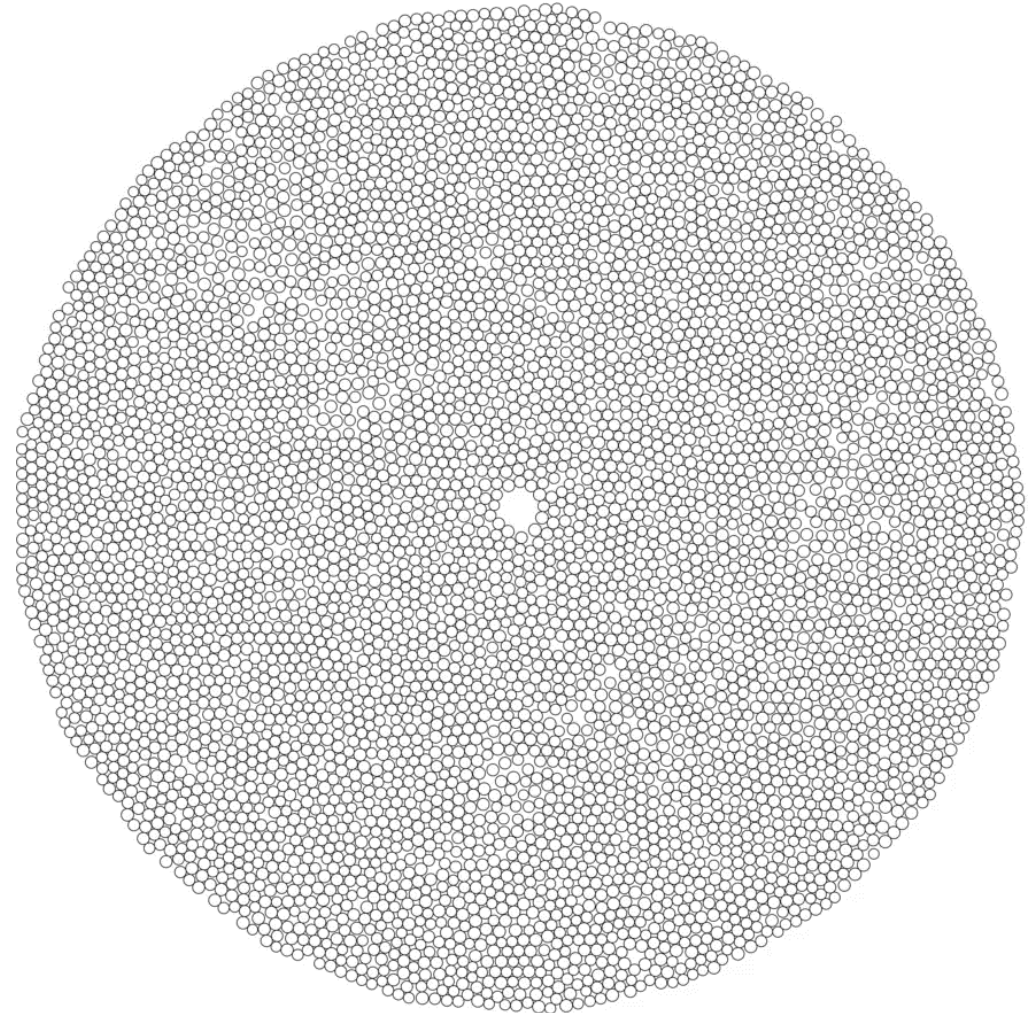
# Jamming transition: force chains “lock-in” ?

force chain network at jamming transition



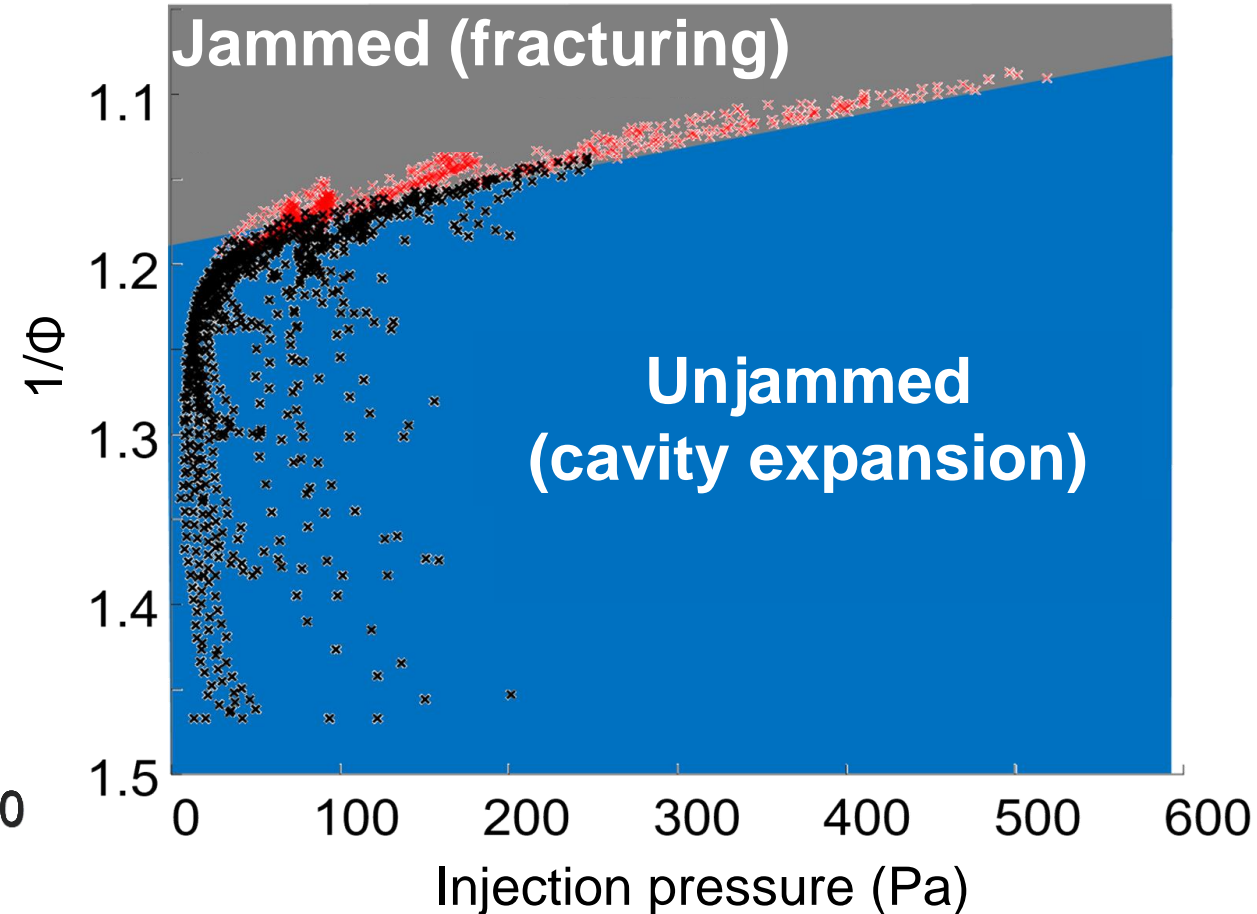
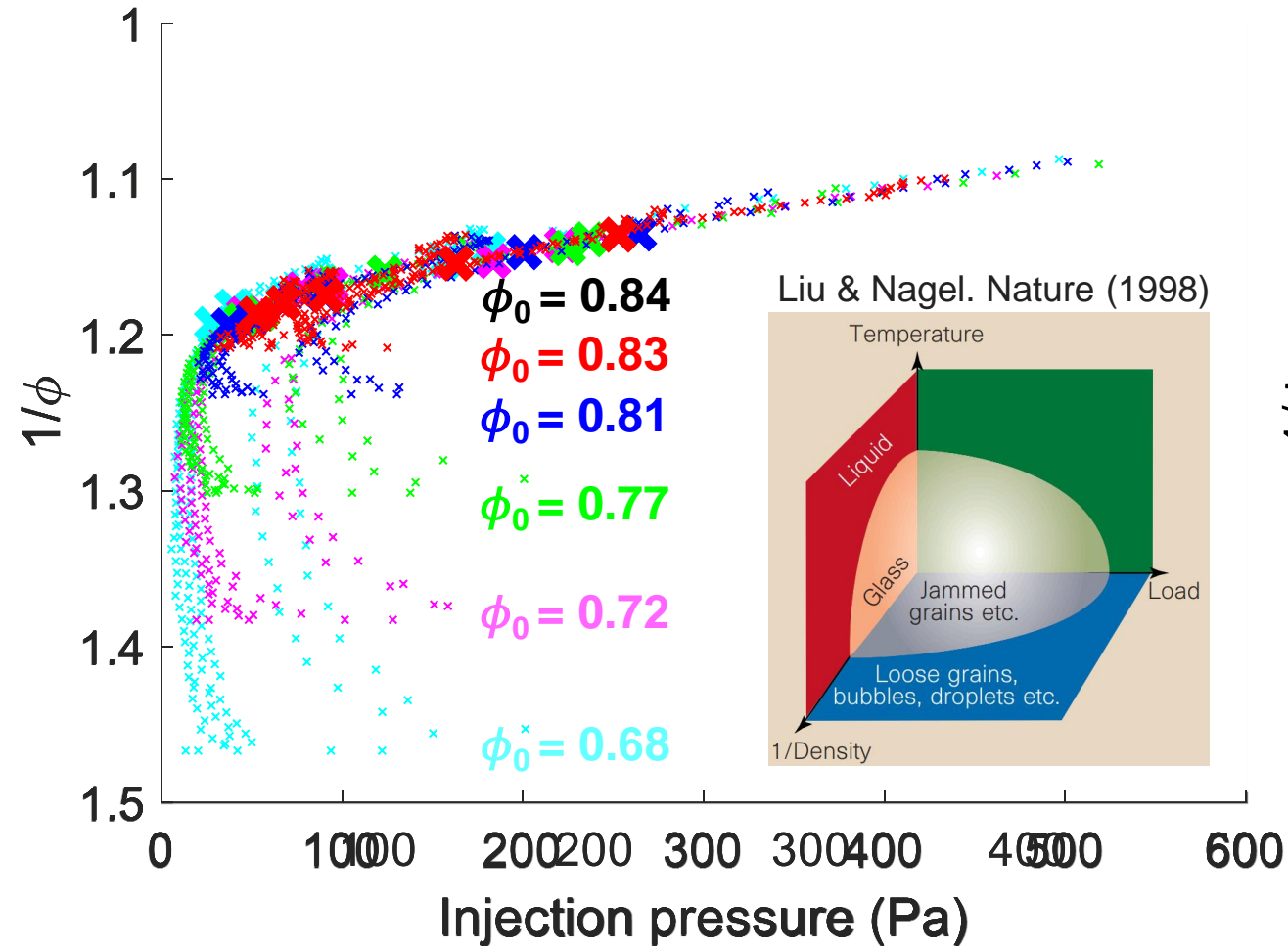
$$\phi_0 = 0.77$$

$$\theta = 140^\circ$$

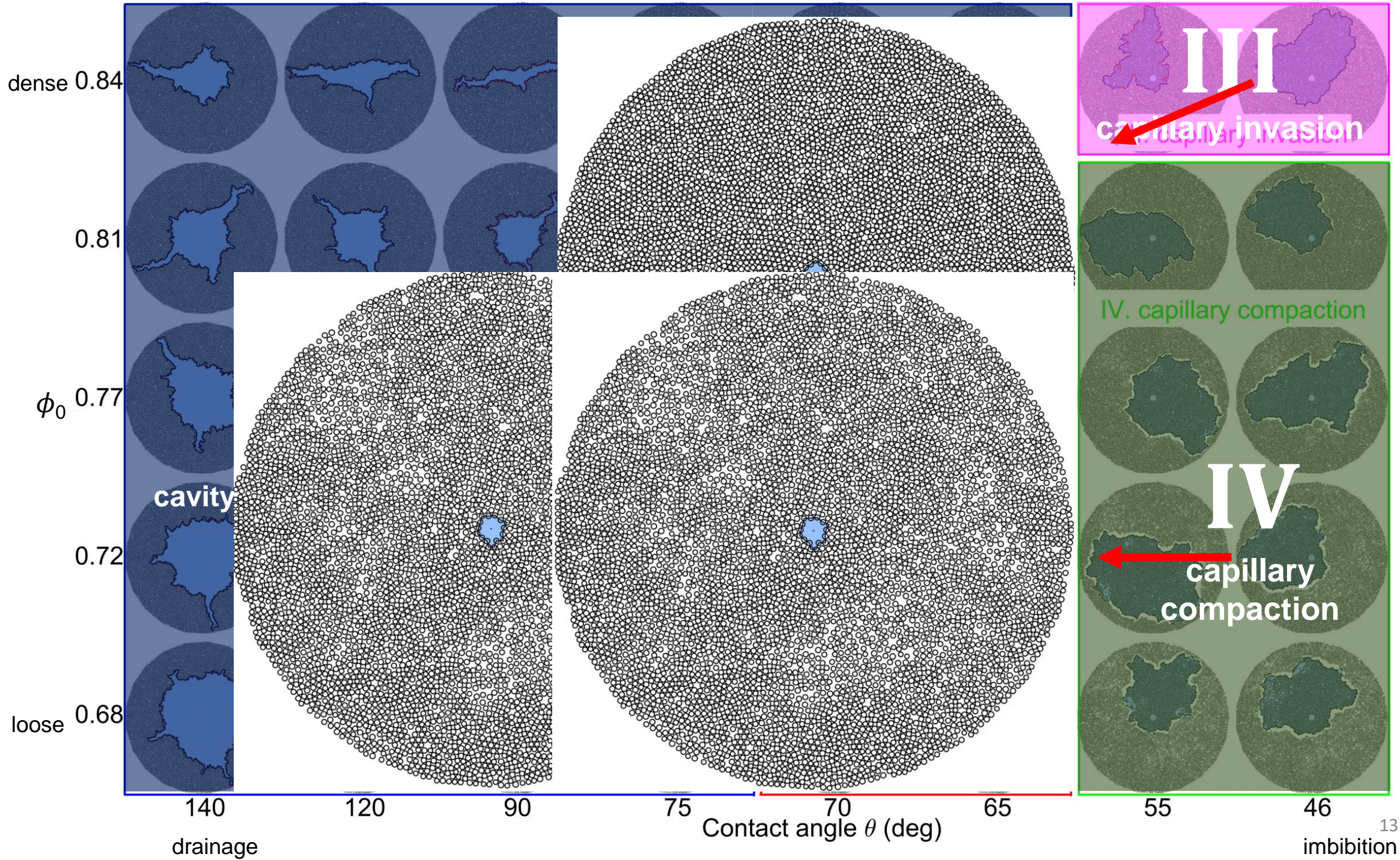


- Jamming transition: the system reaches “mechanical stability”: force chains “lock-in”

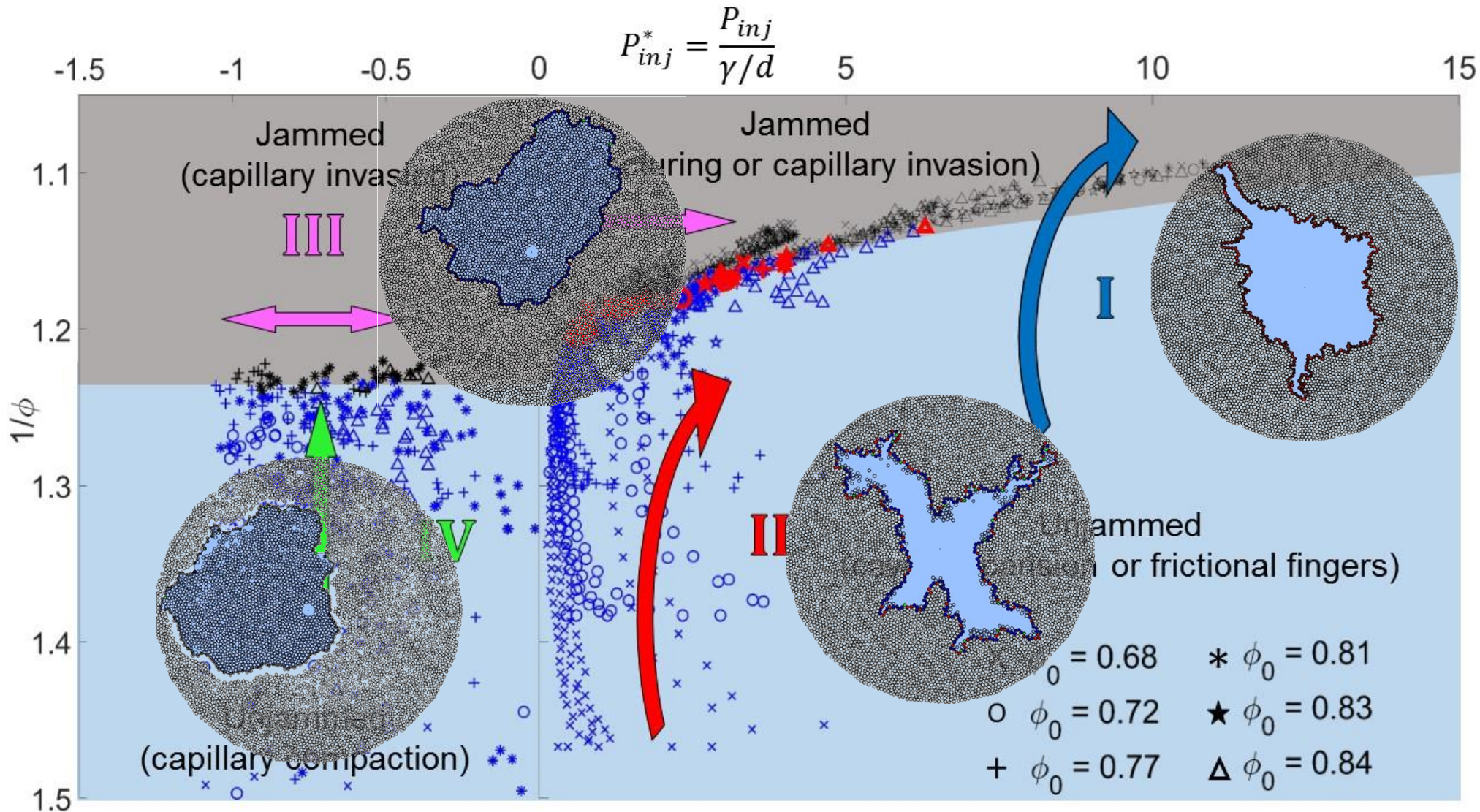
# Trajectories in phase space ( $p_{inj}, 1/\phi$ ): different initial packings



□ **Key result:** the transitions to fracturing for all  $(\theta, \phi_0)$  collapse on a single line in  $(p_{inj}, 1/\phi)$ -space



# Phase diagram of jamming for wet granular media



Y. Meng et al.,  
Physical Review Research (2020)